

ENGINEERS : MAIN STREET FIRE PROTECTION. (801) 830-3856.
ADDRESS : 9959 N Meadow Lane, Highland UT 84003.

LICENSE :
DESIGNER : Kent Johnston
DATE : 11-27-2020

FILE : C:\HYDRON59\La Caille Attic.HYD
JOB NAME : La Caille Attic
LOCATION : 9565 S Wasatch Boulevard Sandy, Utah

DESIGN DATA.

HAZARD :	LIGHT HAZARD ATTIC
DENSITY :	0.134 Sq Ft
AREA PER SPRINKLER :	112 Sq Ft
TOTAL CALCULATED AREA :	1456 Sq Ft
TOTAL SPRINKLERS CALCULATED :	13 Heads

FLOW DATA.

TOTAL SPRINKLER FLOW :	261.8 Gpm
TOTAL HOSE STREAM :	100.0 Gpm
TOTAL WATER REQUIRED :	361.8 Gpm
BASE OF RISER NODE :	RB
FLOW :	261.8 Gpm
PRESS :	50.3 Psi

AUTHORITY HAVING JURISDICTION : Draper UFA
PHONE :

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SOURCE | STATIC : 115 Psi RESIDUAL : 102 Psi FLOW : 1245 Gpm

NODE NO.	ELEVATION Feet	K-FACTOR	PRESSURE Psi	DISCHARGE Gpm
1	16.0	5.60	7.0	14.8
2	16.0	5.60	7.9	15.7
3	16.0		10.9	
4	16.0	5.60	7.9	15.7
5	16.0	5.60	7.0	14.8
6	15.0		13.2	
7	16.0	5.60	7.5	15.3
8	16.0	5.60	8.4	16.3
9	16.0		11.7	
10	16.0	5.60	8.4	16.3
11	16.0	5.60	7.5	15.3
12	15.0		14.1	
13	15.0		19.1	
14	16.0		23.3	
15	16.0	5.60	23.5	27.2
16	16.0	5.60	23.9	27.4
17	10.0		32.5	
18	10.0		35.3	
19	10.0		40.7	
20	10.0		44.4	
21	10.0		44.6	
22	10.0		44.6	
23	16.0	5.60	25.2	28.1
24	16.0	5.60	24.3	27.6
25	16.0	5.60	23.8	27.3
RT	10.0		45.4	
RB	0.0		50.3	
CONN	0.0	SOURCE	52.2	361.8

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SPRINKLERS FLOWING	:	13	Heads
AREA PER SPRINKLER	:	112	Sq Ft
MIN SPRINKLER FLOW	:	15	Gpm
REQUIRED DENSITY	:	0.134	Gpm/Sq Ft
COMPUTED DENSITY	:	0.132	Gpm/Sq Ft

TOTAL SPRINKLER FLOW	:	261.8	Gpm
INSIDE HOSE STREAM	:		Gpm
OUTSIDE HOSE STREAM	:	100	Gpm
TOTAL WATER REQUIRED	:	361.8	Gpm
TOTAL SPRINKLER PRESS	:	52.2	Psi
FIXED PRESS LOSS	:	0.0	Psi

SUPPLY PRESS AVAILABLE	:	113.7	Psi
DEMAND PRESS REQUIRED	:	52.2	Psi
PRESSURE CUSHION	:	61.5	Psi
MAXIMUM VELOCITY	:	18.6	F/S

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Hydronics Engineering
34119 Fremont Bl, Suite 609
Fremont, CA 94555
(800) 845-9819

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PIPE NO.	BEG END	ELEV (Feet) ELEV	FLOW Gpm	K-FACTOR FITTING TYPE DIAMETER	LENGTH FTG TOTAL	C-FACTOR FRI-LOSS (Psi/Ft)	PRESSURE (Psi)		
1	1	16.0	q= 14.8	K= 5.60 L=	14.0		Pt	7.0	Pt 7.0
			Q= 14.8	F= F=	0.0	C= 120	Pe	0.0	Pv -0.2
			Vel= 5.1	D= 1.089 TL=	14.0	0.0622	Pf	0.9	Pn 6.8
2	2	16.0					Pt	7.9	
			q= 15.7	K= 5.60 L=	7.0		Pt	7.9	Pt 7.9
			Q= 30.5	F= T F=	6.0	C= 120	Pe	0.0	Pv -0.7
3	3	16.0	Vel= 10.5	D= 1.089 TL=	13.0	0.2367	Pf	3.1	Pn 7.1
							Pt	10.9	
			q= 14.8	K= 5.60 L=	14.0		Pt	7.9	Pt 7.9
4	4	16.0	Q= 14.8	F= F=	0.0	C= 120	Pe	0.0	Pv -0.2
			Vel= 5.1	D= 1.089 TL=	14.0	0.0622	Pf	0.9	Pn 7.7
							Pt	7.0	
5	3	16.0	q= 15.7	K= 5.60 L=	7.0		Pt	10.9	Pt 10.9
			Q= 30.5	F= T F=	6.0	C= 120	Pe	0.0	Pv -0.7
			Vel= 10.5	D= 1.089 TL=	13.0	0.2367	Pf	3.1	Pn 10.2
6	4	16.0					Pt	7.9	
			q= 0.0	K= 0.00 L=	1.0		Pt	10.9	Pt 10.9
			Q= 61.0	F= T F=	7.0	C= 120	Pe	0.4	Pv -1.0
7	6	15.0	Vel= 12.4	D= 1.420 TL=	8.0	0.2343	Pf	1.9	Pn 9.9
							Pt	13.2	
			q= 0.0	K= 0.00 L=	8.0		Pt	13.2	Pt 13.2
8	6	15.0	Q= 61.0	F= F=	0.0	C= 120	Pe	0.0	Pv -0.6
			Vel= 9.1	D= 1.650 TL=	8.0	0.1128	Pf	0.9	Pn 12.6
							Pt	14.1	
9	7	16.0	q= 15.3	K= 5.60 L=	14.0		Pt	7.5	Pt 7.5
			Q= 15.3	F= F=	0.0	C= 120	Pe	0.0	Pv -0.2
			Vel= 5.3	D= 1.089 TL=	14.0	0.0663	Pf	0.9	Pn 7.3
10	8	16.0					Pt	8.4	
			q= 16.3	K= 5.60 L=	7.0		Pt	8.4	Pt 8.4
			Q= 31.6	F= T F=	6.0	C= 120	Pe	0.0	Pv -0.8
11	9	16.0	Vel= 10.9	D= 1.089 TL=	13.0	0.2525	Pf	3.3	Pn 7.6
							Pt	11.7	
			q= 15.3	K= 5.60 L=	14.0		Pt	8.4	Pt 8.4
12	10	16.0	Q= 15.3	F= F=	0.0	C= 120	Pe	0.0	Pv -0.2
			Vel= 5.3	D= 1.089 TL=	14.0	0.0663	Pf	0.9	Pn 8.2
							Pt	7.5	

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10	9	16.0	q= 16.3	K= 5.60 L=	7.0		Pt	11.7	Pt	11.7
			Q= 31.6	F= T F=	6.0	C= 120	Pe	0.0	Pv	-0.8
			Vel= 10.9	D= 1.089 TL=	13.0	0.2525	Pf	3.3	Pn	10.9
	10	16.0					Pt	8.4		
11	9	16.0	q= 0.0	K= 0.00 L=	1.0		Pt	11.7	Pt	11.7
			Q= 63.2	F= T F=	7.0	C= 120	Pe	0.4	Pv	-1.1
			Vel= 12.8	D= 1.420 TL=	8.0	0.2500	Pf	2.0	Pn	10.6
	12	15.0					Pt	14.1		
12	12	15.0	q= 0.0	K= 0.00 L=	12.0		Pt	14.1	Pt	14.1
			Q= 124.2	F= F=	0.0	C= 120	Pe	0.0	Pv	-2.3
			Vel= 18.6	D= 1.650 TL=	12.0	0.4201	Pf	5.0	Pn	11.8
	13	15.0					Pt	19.1		
13	13	15.0	q= 0.0	K= 0.00 L=	2.0		Pt	19.1	Pt	19.1
			Q= 124.2	F= T F=	9.0	C= 120	Pe	-0.4	Pv	-2.3
			Vel= 18.6	D= 1.650 TL=	11.0	0.4201	Pf	4.6	Pn	16.8
	14	16.0					Pt	23.3		
14	14	16.0	q= 27.2	K= 5.60 L=	7.0		Pt	23.3	Pt	23.3
			Q= 63.1	F= F=	0.0	C= 120	Pe	0.0	Pv	-0.2
			Vel= 5.3	D= 2.203 TL=	7.0	0.0294	Pf	0.2	Pn	23.1
	15	16.0					Pt	23.5		
15	15	16.0	q= 27.2	K= 5.60 L=	7.0		Pt	23.5	Pt	23.5
			Q= 90.2	F= F=	0.0	C= 120	Pe	0.0	Pv	-0.4
			Vel= 7.6	D= 2.203 TL=	7.0	0.0570	Pf	0.4	Pn	23.1
	16	16.0					Pt	23.9		
16	16	16.0	q= 27.4	K= 5.60 L=	30.0		Pt	23.9	Pt	23.9
			Q= 117.6	F= 3ET F=	35.0	C= 120	Pe	2.6	Pv	-0.7
			Vel= 9.9	D= 2.203 TL=	65.0	0.0930	Pf	6.0	Pn	23.3
	17	10.0					Pt	32.5		
17	17	10.0	q= 0.0	K= 0.00 L=	30.0		Pt	32.5	Pt	32.5
			Q= 117.6	F= F=	0.0	C= 120	Pe	0.0	Pv	-0.7
			Vel= 9.9	D= 2.203 TL=	30.0	0.0930	Pf	2.8	Pn	31.9
	18	10.0					Pt	35.3		
18	18	10.0	q= 0.0	K= 0.00 L=	30.0		Pt	35.3	Pt	35.3
			Q= 117.6	F= 2ET F=	28.0	C= 120	Pe	0.0	Pv	-0.7
			Vel= 9.9	D= 2.203 TL=	58.0	0.0930	Pf	5.4	Pn	34.7
	19	10.0					Pt	40.7		

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19	19	10.0	q= 0.0	K= 0.00 L=	78.0		Pt	40.7	Pt	40.7
			Q= 117.6	F= ET F=	30.0	C= 120	Pe	0.0	Pv	-0.3
			Vel= 6.6	D= 2.703 TL=	108.0	0.0343	Pf	3.7	Pn	40.4
	20	10.0					Pt	44.4		
20	20	10.0	q= 0.0	K= 0.00 L=	25.0		Pt	44.4	Pt	44.4
			Q= 117.6	F= T F=	29.0	C= 120	Pe	0.0	Pv	0.0
			Vel= 2.6	D= 4.310 TL=	54.0	0.0035	Pf	0.2	Pn	44.4
	21	10.0					Pt	44.6		
21	21	10.0	q= 0.0	K= 0.00 L=	6.5		Pt	44.6	Pt	44.6
			Q= 144.1	F= F=	0.0	C= 120	Pe	0.0	Pv	-0.1
			Vel= 3.2	D= 4.310 TL=	6.5	0.0052	Pf	0.0	Pn	44.5
	22	10.0					Pt	44.6		
22	22	10.0	q= 28.1	K= 5.60 L=	82.5		Pt	44.6	Pt	44.6
			Q= 144.1	F= 4ET F=	42.0	C= 120	Pe	2.6	Pv	-1.0
			Vel= 12.1	D= 2.203 TL=	124.5	0.1354	Pf	16.9	Pn	43.6
	23	16.0					Pt	25.2		
23	23	16.0	q= 27.6	K= 5.60 L=	9.0		Pt	25.2	Pt	25.2
			Q= 116.0	F= F=	0.0	C= 120	Pe	0.0	Pv	-0.6
			Vel= 9.8	D= 2.203 TL=	9.0	0.0907	Pf	0.8	Pn	24.5
	24	16.0					Pt	24.3		
24	24	16.0	q= 27.3	K= 5.60 L=	10.0		Pt	24.3	Pt	24.3
			Q= 88.4	F= F=	0.0	C= 120	Pe	0.0	Pv	-0.4
			Vel= 7.4	D= 2.203 TL=	10.0	0.0548	Pf	0.5	Pn	24.0
	25	16.0					Pt	23.8		
25	14	16.0	q= 27.3	K= 5.60 L=	3.5		Pt	23.3	Pt	23.3
			Q= 61.1	F= T F=	14.0	C= 120	Pe	0.0	Pv	-0.2
			Vel= 5.1	D= 2.203 TL=	17.5	0.0277	Pf	0.5	Pn	23.1
	25	16.0					Pt	23.8		
26	21	10.0	q= 0.0	K= 0.00 L=	20.0		Pt	44.6	Pt	44.6
			Q= 261.7	F= T F=	29.0	C= 120	Pe	0.0	Pv	-0.2
			Vel= 5.8	D= 4.310 TL=	49.0	0.0155	Pf	0.8	Pn	44.4
	RT	10.0					Pt	45.4		
27	RT	10.0	q= 0.0	K= 0.00 L=	10.0		Pt	45.4	Pt	45.4
			Q= 261.7	F= AC F=	32.0	C= 120	Pe	4.3	Pv	-0.2
			Vel= 5.8	D= 4.310 TL=	42.0	0.0155	Pf	0.7	Pn	45.1
	RB	0.0					Pt	50.3		

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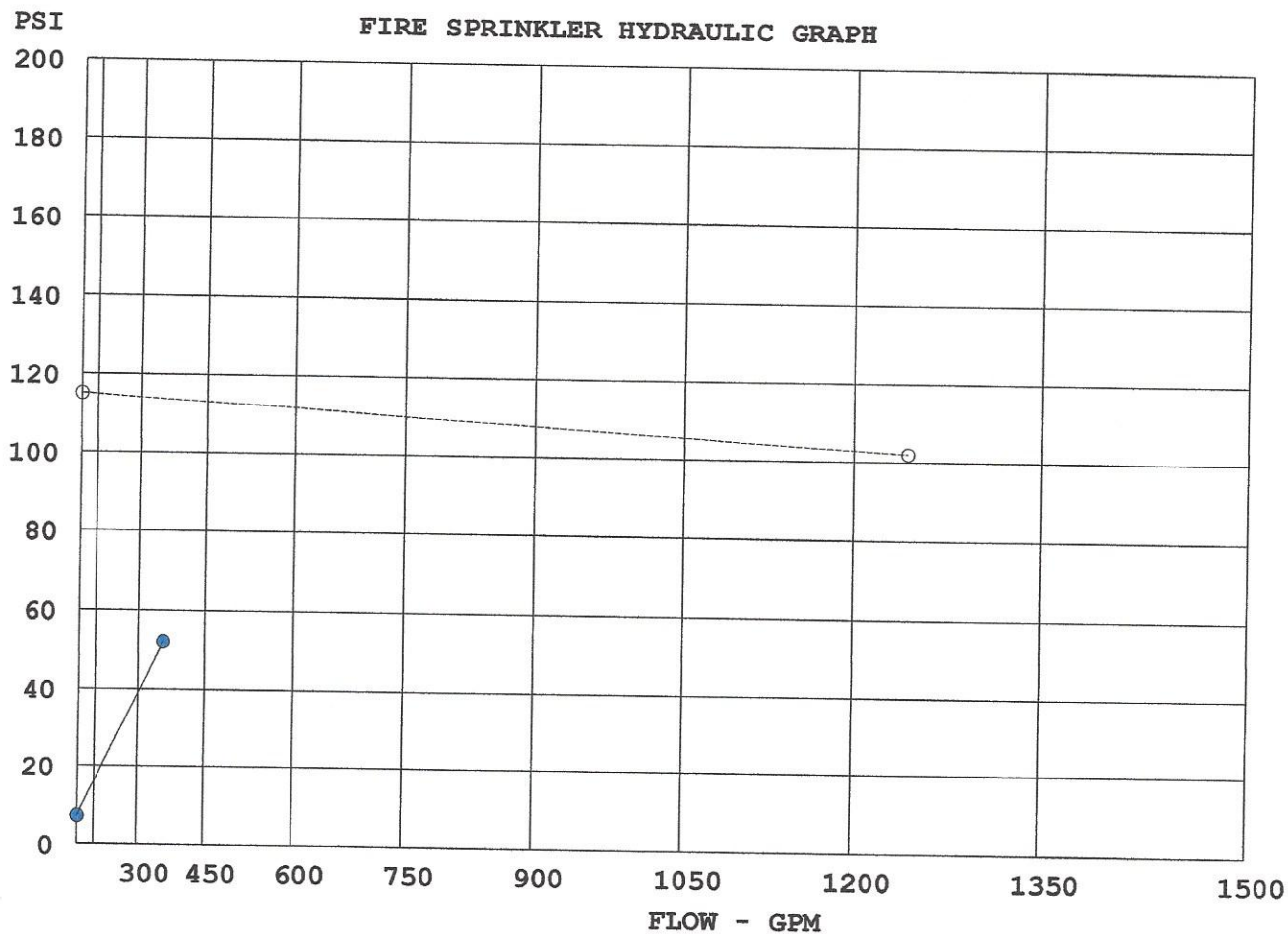
DATE: 11-27-2020 FILE: C:\HYDRON59\La Caille Attic.HYD

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28	RB	0.0	q= 0.0	K= 0.00 L=	110.0	Pt 50.3 Pt 50.3	
			Q= 261.7	F= ET F=	40.0	C= 140 Pe 0.0 Pv -0.2	
			Vel= 5.8	D= 4.280 TL=	150.0	0.0121 Pf 1.8 Pn 50.1	
	CONN	0.0				Pt 52.2	
			Q= 361.8	<<< SOURCE >>>		Pt 52.2	

E=90-Elb T=Tee L=LgtElb C=ChkVlv B=BfyVlv G=GatVlv A=AlmChk F=45-E

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○-----○ Water Supply

Static : 115 Psi
Resid : 102 Psi
Flow : 1245 Gpm

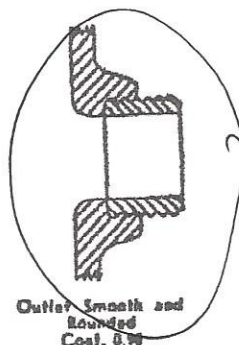
●-----● Water Demand

Avl Press : 113.7 Psi @ 362 Gpm
Req Press : 52.2 Psi @ 362 Gpm
Press Cush: 61.5 Psi

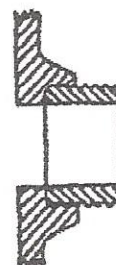
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(800) 845-9819.

FLOW TEST DATA SHEET

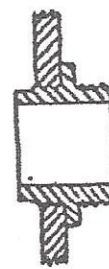
CITY SANDY CITY (UNINCORPORATED) SECTION _____
 NAME OF PROPERTY LA CAILLE RESTAURANT
 ADDRESS 9565 SO. WASATCH BLVD. SANDY, UTAH
 STATE UTAH
 DATE 11/25/20
 TIME 11:00 A.M.
 TEMPERATURE 35° ±
 TYPE OF CITY SYSTEM
 GRAVITY _____
 PUMPS _____
 COMBINATION X



Outlet Smooth and Rounded
Coef. 0.70



Outlet Square and Sharp
Coef. 0.60



Outlet Square & Projecting into B
Coef. 0.70

Fig. 12-12. Three general types of hydrant outlets and their coefficients of discharge

NOTES:

① FLOWED HYDRANT ON PROPERTY. ② FIRE SPER MAIN COMES OFF 6/8" MAIN BETWEEN STATIC READING AND FLOW HYD.

TEST CONDUCTED BY: KENT JOHNSTON FIRE SUPPRESSION SERVICES

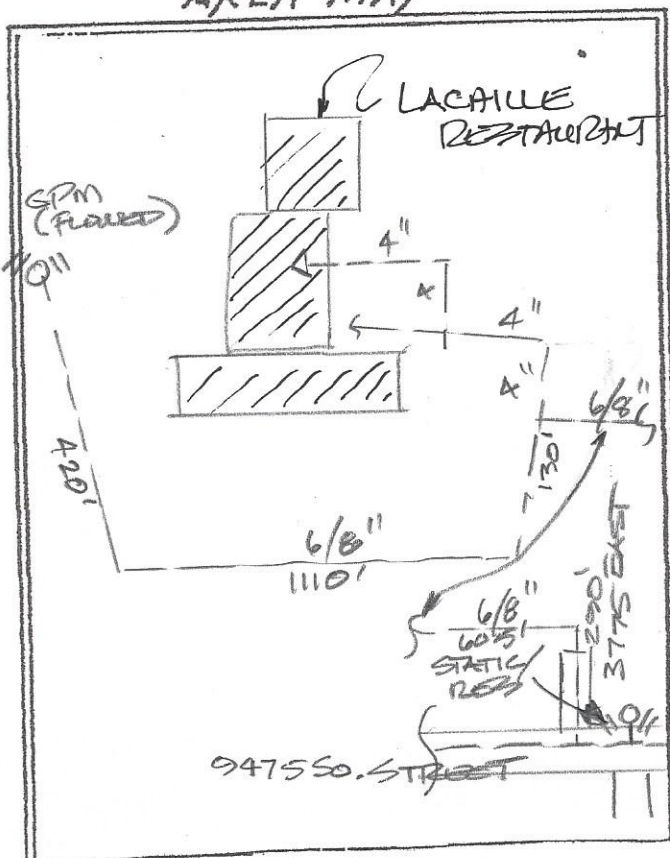
WITNESSED BY: KENT JOHNSTON GERALD STREBEL (SANDY F.D.)

INFO. DIST. TO: SANDY CITY FIRE DEPT. STEWART GRAY (UFA)

DENVER CITY -

$$\text{HAZENWILLIAMS } 29.83 \times .9 \times 6.25 \times \sqrt{55(\text{ft})} = 1245 \text{ GPM}$$

AREA MAP



OUTLET #1. SIZE 2.2

	GAGE #	DIRECT P.S.I.	ADJUSTED P.S.I.	FLOW	OUTLET COEF.	ADJUSTED FLOW
STATIC		115				
RESID.		102				
PITOT		55				1245
SUB.TOT.						

OUTLET #2 SIZE

	GAGE #	DIRECT P.S.I.	ADJUSTED P.S.I.	FLOW	OUTLET COEF.	ADJUSTED FLOW
STATIC						
RESID.						
PITOT						
SUB.TOT.						

ADJUSTED TOTALS

STATIC _____
 RESID _____

